Amendments to the Claims:

The following listing of claims replaces all prior versions and listings of the claims in this application.

Listing of the Claims:

1. (Currently Amended): A process for producing a poly(arylene sulfide), comprising, after a dehydration step of heating and dehydrating a mixture containing an organic amide solvent, at least one sulfur source (A) selected from the group consisting of alkali metal hydrosulfides and alkali metal sulfides, and an alkali metal hydroxide added as needed to control the amount of water in the mixture, a polymerization step of charging a dihalo-aromatic compound (B) into the system containing the remaining mixture to subject the sulfur source (A) and the dihalo-aromatic compound (B) to a polymerization reaction in the organic amide solvent, which comprises:

(1) in the dehydration step, (i) heating the mixture containing the organic amide solvent, at least one sulfur source (A) selected from the group consisting of alkali metal hydrosulfides and alkali metal sulfides, and the alkali metal hydroxide added as needed in a reaction vessel, to which a distillation column is linked, and guiding volatilized vapor volatilized to the distillation column to distill and separate it into respective components, (ii) refluxing a fraction taken out of the bottom of the distillation column and comprising the organic amide solvent as a principal component into the reaction vessel, (iii) cooling a fraction taken out of the top of the distillation column and comprising water and hydrogen sulfide to discharge hydrogen sulfide that is not condensed by the cooling and reflux a part of water condensed into the distillation column, and (iv) discharging the remaining water, wherein a weight ratio of an amount of water refluxed into

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the distillation column in step (iii) to an amount of water discharged without being refluxed in step (iv) is within a range of from 90:10 to 10:90,

- (2) determining a relational expression between the total amount of water of an amount of water refluxed into the distillation column and an amount of water discharged without being refluxed, and an amount of hydrogen sulfide discharged from the reaction vessel in advance, thereby calculating out an amount of hydrogen sulfide discharged from the reaction vessel from a measured value of the total amount of water on the basis of the relational expression, calculating an amount of hydrogen sulfide discharged from the reaction vessel on the basis of a relational expression between the total of the amount of water refluxed into the distillation column in step (1)(iii) and the amount of water discharged without being refluxed in step (1)(iv), and the amount of hydrogen sulfide discharged from the reaction vessel, wherein the relational expression is predetermined by regression analysis using experimental data actually measured as to the relation between the total amount of water and the amount of hydrogen sulfide volatilized out in the dehydration step as a database,
- (3) calculating out an amount (hereinafter referred to as "amount of the sulfur source charged") of the sulfur source (A) remaining in the mixture after the dehydration step on the basis of the <u>calculated</u> amount of <u>discharged</u> hydrogen sulfide calculated out, thereby and controlling a charged molar ratio of the sulfur source (A) to the dihalo-aromatic compound (B) on the basis of the amount of the sulfur source (A) calculated out, and then
- (4) subjecting the sulfur source (A) and the dihalo-aromatic compound (B) to the polymerization reaction in the organic amide solvent in the polymerization step.

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2. (Currently Amended) The production process according to claim 1, wherein the relational expression is a linear relational expression represented by the following relational expression (I):

$$y = ax + b$$
 (I)

wherein x is the total amount of the amount of water refluxed into distillation column and the amount of water discharged without being refluxed in the dehydration step, y is the amount of hydrogen sulfide discharged from the reaction vessel, and both a and b are parameters.

- 3. (Original) The production process according to claim 1, wherein in the dehydration step, the mixture is heated to a temperature of 100 to 250°C.
 - 4. (Canceled).
- 5. (Original) The production process according to claim 1, wherein in the dehydration step, the dehydration under heat is conducted in such a manner that the water content falls within a range of 0.3 to 5 mol per mol of the alkali metal sulfide (A) charged.
- 6. (Original) The production process according to claim 1, wherein in the dehydration step, the dehydration under heat is conducted by means of an apparatus so constructed that an upper part of the reaction vessel is connected to the distillation column, a fraction from the top of the distillation column is successively sent to a condenser and a storage tank, a fraction from the bottom of the distillation column is refluxed into the reaction vessel, a part of water stored in the

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storage tank is refluxed into the distillation column, and at that time an amount of water refluxed

is integrated by a flowmeter.

7. (Original) The production process according to claim 1, wherein after the dehydration

step, an amount of the dihalo-aromatic compound (B) charged is controlled within a range of

1.00 to 1.09 mol per mol of the sulfur source (A) charged.

8. (Currently Amended) The production process according to claim 1, wherein in the

polymerization step, the polymerization reaction is conducted by an at least two-stage

polymerization process comprising:

(1) Step 1 of heating a reaction mixture containing the organic amide solvent, the sulfur

source (A) and the dihalo-aromatic compound (B) to 170 to 270°C in the presence of water in an

amount of 0.5 to 2.0 mol per mol of the sulfur source (A) charged to conduct a polymerization

reaction, thereby forming a prepolymer that a wherein conversion of the dihalo-aromatic

compound is 50 to 98%, and

(2) Step 2 of controlling the amount of water in the reaction system so as to bring about a

state that water exists in a proportion of more than 2.0 mol, but up to 10 mol per mol of the

sulfur source (A) charged, and heating the reaction system to 245 to 290°C, thereby continuing

the polymerization reaction.

9. (Original) The production process according to claim 8, wherein in Step 1, a

prepolymer having a melt viscosity of 0.5 to 30 Pa·s as measured at a temperature of 310°C and

a shear rate of 1,216 sec⁻¹ is formed.

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